Magnetic resonance imaging as a tool to assess reliability in simulating hemodynamics in cerebral aneurysms with a dedicated computational fluid dynamics prototype: preliminary results

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Purpose: As an example of enhancing information in clinical image data by computational methods, simulating hemodynamics in cerebral aneurysms by means of computational fluid dynamics (CFD) is currently a topic of active research. Challenges consist in translating this engineering technology into clinical research, validating the simulations and addressing a potential clinical value of the results. In this preliminary study, we demonstrate the use of phase contrast magnetic resonance imaging (pcMRI) for assessing the reliability of CFD results. **Materials and methods:** For six cerebral aneurysms where intra-aneurysmal velocity information was available by

2D pcMRI, steady CFD simulations with constant inflow were performed using a dedicated CFD prototype system. Major features of the velocity patterns derived from pcMRI were compared to those obtained with the CFD.

Results: Good qualitative agreement between measured (2D pcMRI) and simulated (CFD) features of the intra-aneurysmal velocity patterns were obtained. These findings are discussed in the broader framework of the expectations towards CFD simulations in a clinical research setting.

Conclusions: Computational simulations reproduce major features of measured velocity patterns in cerebral aneurysms. Looking forward, these simulations need to be refined towards specific applications in clinical research.

Keywords: Cerebral aneurysms; computational fluid dynamics (CFD); aneurysm rupture

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Introduction

The concept of using medical image data for the creation of computational models and the subsequent simulation of hemodynamics in these models has been expressed already almost 20 years ago (1,2). Around a decade ago, this concept was revived mainly because of the progress in computational hardware which enables the researcher to now conduct these simulations on personal computer workstation with cost-effective, versatile software that is flexible enough to be used with computational models derived from medical image data for a specific patient (3). Since then, a variety of studies have been published exploring the feasibility of using computational fluid dynamics (CFD) for the simulation and quantification of aneurysm hemodynamics as well as investigating its usefulness for therapeutic applications.

In cerebral aneurysms, geometrical properties of the parent artery (4-6) were reported to influence the simulation results as did variations in the inflow waveform of the boundary conditions (7,8), and the duration of the simulated cardiac cycle (9). Hemodynamic conditions in the parent artery were potentially associated with aneurysm formation (10) as were hemodynamics values in the aneurysm itself with risk of rupture (11-14). Validation of simulation results was attempted using fluoroscopic angiographic images (15,16) or phase contrast magnetic resonance imaging (pcMRI). For the latter, first 2D methods were explored (17,18) and, later, the time-dependent velocity fields obtained with the novel 4D pcMRI methods were correlated with corresponding quantities obtained with the CFD simulations (19,20). In addition, CFD methods have been employed to investigate the potential of this technique for predicting hemodynamics changes and to explain different outcome after endovascular treatment with the novel flow diverter devices (21-23).

All these efforts contributed to translating CFD as an engineering technology into a clinical research tool. While the high potential of CFD for the quantification and visualization of cerebral aneurysm hemodynamics has been established in the last decade, recent discussions show that a better understanding and a thorough validation of this technique is needed, before its potential value for therapeutic decisions can be assessed (24-26). In addition to validating software performance and reproducibility of simulation results, it is important to understand limitations for the application of these simulation techniques to *in vivo* data. In this study we compare measurements of velocity patterns using a 2D phase contrast magnetic resonance method with results of a novel CFD prototype system.

Materials and methods

2D pcMRI

The 2D pcMRI images were acquired at a 1.5 T MRI scanner (Siemens AG, Erlangen) from six patients diagnosed with a cerebral aneurysm. From a 3D time-of-flight (TOF) scan, which was acquired as a localizer (FOV 220 mm, matrix: 512×256, slice thickness: 0.5 mm), cross-sectional planes intersecting each aneurysm at approximately two perpendicular orientations were selected. Dependent on the length of the cardiac cycle, 12-20 pcMRI images per cardiac cycle were obtained using a peripheral monitor and a retrospective gating approach [FOV 160 mm, slice thickness 5 mm, matrix: 256×192, velocity-encoding (VENC) values, perpendicular to scan plane only, ranged from 60-150 cm/s]. Images at systole were selected for comparison with CFD results.

CFD simulations

CFD, as a branch of fluid dynamics, utilizes numerical methods to solve problems which involve fluid flows. Computational algorithms which approximate the real system and which use boundary conditions that define the geometry, the inflow and outflow parameters of the model, calculate the velocity vector field and other derived hemodynamic parameters such as pressures and wall shear stresses, i.e., forces, which the fluid exerts onto the wall. As a first step in this process, the physical bounds of the computational model are defined. This so defined volume is then divided into small elements (cells) that constitute the computational mesh. The governing physical equations, for this case, the Navier-Stokes equations, are then iteratively solved on the computational mesh taking into consideration the boundary conditions. Postprocessing software is then utilized for further analysis and visualization.

IRB approval was obtained for this study. The 3D digital angiography subtraction (DSA) image data, originally acquired during a diagnostic angiogram, were retrospectively collected for the six aneurysms. Image data was transferred to the dedicated workstation of a CFD research prototype (Siemens AG, Figure 1). While clientserver systems have been recently described as a model for integration into the clinical workflow (27), the CFD research prototype described here consisted of standalone software installed on a single workstation with computational power similar to a personal computer. The software as well as the entire prototype is currently developed as a research tool and not part of any commercial clinical software package. An optimized algorithm consisting of different parts was utilized to conduct the CFD simulations using this prototype: in part 1, a 3D surface model of the corresponding vasculature was created. In part 2, small arterial branches and venous contamination (if present) were manually eliminated. In part 3, the computational mesh was created after manually defining inflow and outflow regions. In part 4, steady CFD simulations were performed (maximum inflow velocity 0.8 m/s). Using a level-set based embedded boundary method, the Navier-Stokes equations were solved with userspecified boundary conditions (28). Blood was modeled as an incompressible fluid with a density of 1,000 kg/m³ and a viscosity of 0.004 kg/ms. In part 5, simulation results were stored on disk using the visualization toolkit (vtk) file format (Kitware Inc.) and cross sections were defined across the computational model at the same locations as the cross sections measured with 2D pcMRI. At these cross sections, velocity components perpendicular to each cross section were visualized in a similar fashion as the measured velocity components.

Results

In all six cases, generally a good agreement was found between the major flow features in the cross sections calculated with the CFD prototype and measured with 2D



Figure 1 User interface of the dedicated CFD research prototype system for displaying the CFD simulation results of case #1. Cross sections through the aneurysm dome can be easily defined (upper left quadrant). Wall shear stress information can be integrated into 3D surface reconstructions of the vasculature (upper right and lower left quadrant) and streamlines of flow can be shown within the aneurysm dome (lower right quadrant). CFD, computational fluid dynamics.

pcMRI. A more detailed discussion for each case follows (please also refer to *Figure 2*).

Case 1

In the first cross section, the bilobular or dumbbell shape of the aneurysm shows regions of opposite flow directions at the base of the dumbbell relative to both lobes for both simulated and measured data. Qualitatively higher velocities were visible in the simulated case compared to the measurements. The velocity overestimation in the simulation might be due to the assumption of rigid walls, which may be less valid for the lobes, as these were found to exhibit higher wall pulsatility then the main body of the aneurysm (29). In the second cross section, opposite flow directions are visible at the left and right wall indicating a circular blood motion typically found in cerebral aneurysms. Excellent qualitative agreement between the major flow features in this cross section was apparent.

Case 2

Both the simulated as well as the measured data agreed in the overall direction of blood flow, however, the shape and extend of the major flow features differ considerably in both cross sections. Particularly in the second cross section, the area represented by low voxel intensity was underestimated in the simulations.



Figure 2 Cross sections on left were measured (pcMRI) or simulated (CFD) of aneurysms shown on the right. Black patterns and light blue patterns represent blood velocity values of opposite direction relative to the cross sectional plane. Qualitative agreement between simulation and measurement was assessed by similarity in size and shape of the velocity patterns in each cross section. pcMRI, phase contrast magnetic resonance imaging; CFD, computational fluid dynamics.

Case 3

In this large and irregularly shaped aneurysm, major flow features were well represented by the simulation results in comparison to the 2D pcMRI measurements. Low signal to noise in the 2D pcMRI images at regions of slow flow (potentially more pronounced in this large aneurysms compared to the other ones of smaller diameter) were appreciated.

Case 4

Agreement was overall found favorable in the velocity patterns visible in both cross sections between measurement and simulations sections despite some apparent differences towards the aneurysm dome, in particular in the first cross section. Opposite regions of flow were quite distinguishable in the 2D pcMRI inside the entire dome while in the simulation results, a more diffuse, slow flow pattern was attributed to the dome region. In the second cross section, perpendicular to the first, agreement was better concerning the shapes of the velocity patterns while the simulation seemed to underestimate blood flow velocities.

Case 5

In this large aneurysm, focal areas of high velocity blood

flow were well reproduced in the simulation results compared to the measurements. Low signal to noise corresponding to regions of slow velocities were again appreciated similar to case 3.

Case 6

In this aneurysm, which exhibited a thrombosed dome region, velocity patterns agreed very well in the second cross section while also qualitatively moderate to good agreement was found in the first cross section where the CFD simulation overestimated velocity magnitudes.

Discussion

Illustrated by the qualitative comparison of *in vivo* measurements realized by 2D pcMRI and steady-inflow CFD simulations performed with a dedicated CFD prototype, CFD as implemented as a dedicated prototype system is capable of reproducing major flow features in cerebral aneurysms.

The findings of this preliminary results study is in good agreement with previously published work using the commercially available CFD solver software (30). In contrast to a commercial software, which, due to its high flexibility in the kinds of simulations it can perform, most often is of high complexity perhaps unsuitable for easy use in a clinical research setting, the application of the CFD prototype system employed here, was very easy to use for the six described cases. The workflow was predefined and segmentation as well as definition of boundary conditions for the simulations was greatly simplified. As costs of this simplification, currently only zero pressure boundary conditions are available and inflow can only be defined by a velocity value. Thus, no pressure values or a velocity profile defined across the diameter of the parent artery are currently feasible.

In this preliminary results study, steady simulations were chosen as only these are from a practical clinical standpoint sufficiently fast to provide results within the time frame of a diagnostic angiogram or during an endovascular embolization procedure. Despite this simplified approach, the qualitative agreement between simulation and measurement was generally very good in that it provided quickly information for the intra-aneurysmal blood flow patterns. It may be argued that this information may be too cursory and more sophisticated simulations are needed utilizing time-varying inflow (and even perhaps) outflow conditions. To address this issue, it would be also

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necessary to define expectations for the CFD simulation results: while the possibility of calculating an aneurysm rupture risk has been discussed as a potential application for CFD, it should be kept in mind that in addition to geometrical and morphological factors giving rise to mechanical forces (31,32), also other factors, such as current smoking, hypertension, family history of stroke other than subarachnoid hemorrhage, hypercholesterolemia and regular physical exercise have been implicated to attribute to aneurysm rupture risk (33). While hypertension might be related to elevated wall shear stress, a hemodynamic parameter accessible via CFD, it might be difficult to account for the remaining factors in the computational simulations.

Other clinical research applications of CFD have recently been reported which investigate entirely mechanical effects, e.g., the influence of eight different configurations of stenting for bifurcation aneurysms on the hemodynamics inside the aneurysm (34). The authors demonstrated that the crossing-Y and kissing stent configuration lead to lower flow velocity within the aneurysms. In another study, CFD simulations helped to predict the rupture side in subarachnoid hemorrhage in a patient with bilateral vertebral aneurysms in order to decide which aneurysm need to be treated first (35). These are examples of scenarios where CFD was used to address a well-defined clinical research issue, and these kinds of scenarios may be readily addressed by the CFD research prototype describe here.

Conclusions

CFD simulations of cerebral aneurysms is an evolving technology with promising applications in clinical research for the near future. A standardized approach, as realized by the dedicated CFD prototype system described in this study, will be beneficial for comparison and exchange of simulation results.

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