



# Distribution and regional variation of wall shear stress in the curved middle cerebral artery using four-dimensional flow magnetic resonance imaging

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**Background:** To investigate the distribution and regional variation of wall shear stress (WSS) in the curved middle cerebral artery (MCA) in healthy individuals using four-dimensional (4D) flow magnetic resonance imaging (MRI).

**Methods:** A total of 44 healthy participants (18 males; mean ages: 27.16±5.69 years) were included in this cross-sectional study. The WSS parameters of mean, minimum, and maximum values, the coefficient of variation of time-averaged WSS (TAWSS<sub>CV</sub>), and the maximum values of the oscillatory shear index (OSI) were calculated and compared in the curved proximal (M1) segments. Three cross-sectional planes were selected: the location perpendicular to the beginning of the long axis of the curved M1 segment of the MCA (proximal section), the most curved M1 location (curved M1 section), and the location before the insular (M2) segment bifurcation (distal section). The WSS and OSI parameters of the proximal, curved, and distal sections of the curved M1 segment were compared, including the inner and outer curvatures of the curved M1 section.

**Results:** Of the curved M1 segments, the curved M1 section had significantly lower minimum TAWSS values than the proximal (P=0.031) and distal sections (P=0.002), and the curved M1 section had significantly higher maximum OSI values than the distal section (P=0.001). The TAWSS<sub>CV</sub> values at the curved M1 section were significantly higher than the proximal (P=0.001) and distal sections (P<0.001). At the curved M1 section, the inner curvature showed a significantly lower minimum TAWSS (P=0.013) and higher maximum OSI values (P=0.002) than the outer curvature.

**Conclusions:** There are distribution variation of WSS and OSI parameters at the curved M1 section of the curved MCA, and the inner curvature of the curved M1 section has the lowest WSS and highest OSI distribution. The local hemodynamic features of the curved MCA may be related to the predilection for

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atherosclerotic plaque development.

**Keywords:** Wall shear stress (WSS); oscillatory shear index (OSI); middle cerebral artery (MCA); magnetic resonance imaging (MRI); four-dimensional flow imaging

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## Introduction

Hemodynamic factors have been shown to play an important role in the formation and development of vascular diseases, including atherosclerosis (AS), aneurysms, and arteriovenous malformations (AVMs) (1-3). Irregular vascular geometry, including bifurcation, curvature, and branching, can lead to regionally different flow status, which subsequently generates spatial and temporal changes in the shear forces acting on a vessel wall. As a key parameter in cardiovascular hemodynamics, wall shear stress (WSS) (4) expresses the force per unit area exerted by the wall on the blood flow in a direction on the local tangent plane, which is linked to the initiation and progression of many vascular diseases (5-7). The oscillatory shear index (OSI) is a WSS-related parameter that describes the WSS directional changes during the cardiac cycle. It has been well accepted that low WSS and a high OSI represent sensitive markers for the formation of atherosclerotic plaques (8). Previous studies of the aorta, carotid, and coronary arteries have shown that atherosclerotic plaques develop preferentially at curved arteries and near side branches, which are in the regions exposed to disturbed flow and shear stress (9-12).

The proximal (M1) segment of the middle cerebral artery (MCA), which extends from the ending of the internal carotid artery to the first main division of the MCA, is one of the most common locations of intracranial atherosclerotic plaques (13). Although the M1 segment (also termed the horizontal segment) is generally considered straight, it has a curved shape in many cases. Several studies have reported that the MCA geometry is associated with plaque distribution and stroke (14,15). It has been indicated that MCA plaques are preferentially located on the inner wall of the curved MCA (15). One study using computational fluid dynamics (CFD) showed that AS might occur in the middle of a branch of the MCA with the highest geometrical curvature (16). The possible explanation was that the curved MCA affected local hemodynamic status, resulting in the uneven distribution of WSS on the circumferential plane

of the curved MCA. However, to date, few hemodynamic studies have measured the distribution of WSS on the curved MCA *in vivo* before the development of AS.

Four-dimensional (4D) flow magnetic resonance imaging (MRI), which shows the real-time blood flow patterns of individual patients, allows for the *in vivo* quantification and comprehensive assessment of the cardiovascular system. Using this technique, volumetric velocity data can be directly obtained in a three-dimensional (3D) direction during a cardiac cycle period (17). After the flow data are processed, noninvasive qualitative and quantitative assessments can be accurately performed on flow velocity and other hemodynamic parameters, including flow rate, WSS, and pressure, during the entire cardiac cycle. Using this technique, *in vivo* studies have been conducted on patients with congenital heart disease, aorta dilation, and extracranial-intracranial bypass, with favorable and promising results demonstrated (18-20). The reproducibility of this technique has also been verified in previous studies (21,22).

We hypothesized that WSS parameters may be different among the 3 different sections (proximal, curved, and distal) of the long axis of the M1 segment of the curved MCA, and the curved M1 may have a certain shear force spatial distribution at the most curved location. The purpose of this study was to investigate the distribution and regional variation of the WSS of curved MCAs using 4D flow imaging in healthy participants. We present the following article in accordance with the Strengthening the Reporting of Observational Studies in Epidemiology (STROBE) reporting checklist (available at <https://qims.amegroups.com/article/view/10.21037/qims-22-67/rc>).

## Methods

### Participants

This cross-sectional study enrolled 49 healthy participants from Beijing Tiantan Hospital between May 2016 to November 2020. Individuals were excluded if they had

**Table 1** Imaging parameters of MRA and flow imaging

Parameters	Siemens		Philips	
	3D TOF MRA	4D flow MRI	3D TOF MRA	4D flow MRI
TR/TE (ms)	22/3.5	54.96/3.13	21/3.4	8.7/4.1
Flip angle (°)	18	15	17	20
Field of view (mm <sup>2</sup> )	200×200	200×140	200×200	160×160
Matrix size	384×250	208×140	384×250	160×160
Slice thickness (mm)	1.3	1.0	1.3	1.0
Slices	120	36	120	36
Acceleration factor	2	2	2	3
In-plane resolution (mm <sup>2</sup> )	0.52×0.8	1.0×1.0	0.52×0.8	1.0×1.0
Venc (cm/s)	–	120	–	120
Scan time (min)	2–3	11–13	2–3	8–10

MRA, magnetic resonance angiography; 3D TOF MRA, three-dimensional time-of-flight magnetic resonance angiography; 4D flow MRI, four-dimensional flow magnetic resonance imaging; TR, repetition time; TE, echo time; Venc, velocity encoding.

cardiovascular diseases, a history of central nervous system diseases, or vascular risk factors such as hypertension, hyperlipemia, diabetes, smoking, and drinking. Those with claustrophobia or contraindication for MRI examination or scans of poor image quality were also excluded. The study was conducted in accordance with the Declaration of Helsinki (as revised in 2013) and supported by the Institutional Review Board of Beijing Tiantan Hospital, Capital Medical University (No. KY 2019-053-02). Written informed consent was provided by all study participants.

### ***MRI and flow data acquisition***

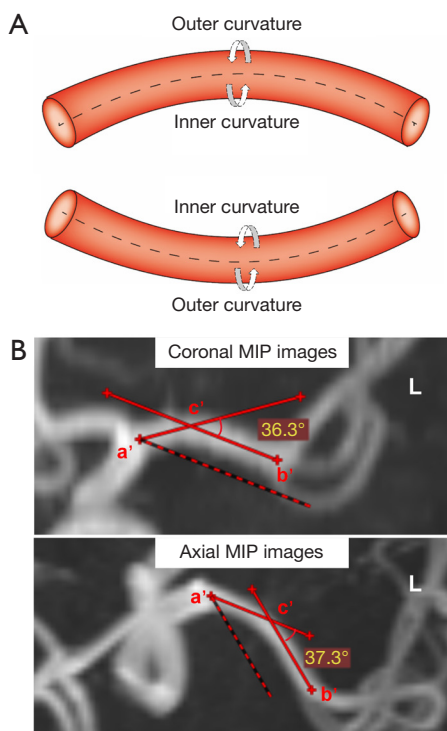
The MRIs were carried out with 3.0 Tesla MR scanners (Trio Tim, Siemens, Erlangen, Germany; Ingenia CX, Philips Healthcare, Best, the Netherlands) with a 32-channel head coil. A 3D time-of-flight (TOF) magnetic resonance angiography (MRA) was performed with maximum intensity projection (MIP) reconstruction to visualize the morphology of the intracranial arteries. Then, 4D flow data were acquired with an oblique coronal orientation, covering the M1 and M2 segments of MCAs, bilaterally. The 4D flow imaging was carried out using the standard generalized autocalibrating partial parallel acquisition (GRAPPA) parallel imaging for the Siemens MR scanner and the accelerated compressed sensing (CS) 4D flow MRI for the Philips MR scanner. All flow data were acquired using prospective and pulse gating, and the scan time was 8–13 min, depending on the heartbeats of the

participants. The parameters of the imaging sequences are listed in *Table 1*.

### ***Definition of the curved M1 segment and the cross-sectional plane setting***

According to the vessel projections on the MIP images of the 3D TOF MRA, the shape of the M1 segment was classified into 3 groups according to a previous study (23): (I) straight; (II) C-shaped; and (III) S-shaped MCA. In order to reduce the influence due to morphological differences of the other 2 types of arteries, only the C-shaped MCA, called the curved MCA, was included and analyzed in this study. On the coronal and axial MRA MIP images, 2 straight lines were drawn through the midline of the target MCA, 1 from the ICA termination (a') to the most curved point (c') and the other from the MCA bifurcation (b') to the most curved point (c') (24). If the intersection angle of these 2 straight lines was larger than 10° on the coronal or axial MRA MIP images, the vessel was defined as a curved-shaped M1 vessel (*Figure 1*).

For each artery, 3 cross-sectional planes with a thickness of 1 mm perpendicular to the long axis of the curved M1 segment were selected and analyzed. The planes were set 1 mm at the distal end of the beginning of the M1 segment (proximal section) and 1 mm before the M2 bifurcation (distal section), respectively. The curved M1 section was selected at the most curved point. As for the curved M1 section, the circumferential wall was divided and described



**Figure 1** Illustrations of the geometry of the curved MCA. The opening orientation of the curved proximal (M1) segment was used to define the inner curvature and outer curvature (A). On the coronal and axial MIP images, the M1 segment was defined as the curved MCA when the intersection angle of the 2 straight lines was larger than 10° (B). MIP, maximum intensity projection; MCA, middle cerebral artery.

as the inner curvature and outer curvature of the curved MCA, according to the opening orientation of the curved M1 segment (15), as shown in *Figure 2*. Then, the planes perpendicular and parallel to the opening orientation were defined separately. The inner curvature and outer curvature were divided along the perpendicular line through the cross-sectional plane. The curved-shaped M1, the curved M1 section, and the inner/outer curvature were independently defined by two observers (Dr. B.X. and Dr. F.M.), and the differences between the two observers were solved by consensus.

**Postprocessing and 3D visualization of 4D flow data**

The time-average images of the 4D flow MRI were obtained by MATLAB software (The MathWorks, Natick, MA, USA). The TOF MRA MIP images were used for

vessel wall segmentation due to the better blood flow signal contrast. The TOF MRA images were registered as 4D flow images using the volumetric rigid registration method (i.e., elastix) in the 3D Slicer ([www.slicer.org](http://www.slicer.org)) image software package to reserve the velocity information in 4D flow MRI. After image registration, the registered TOF images were utilized to generate the visualized 3D vessel model. In detail, algorithms, including threshold segmentation, connected domain selection, surface extraction, and smoothing, were used to segment and reconstruct the 3D triangular-meshed vessel model in our in-house software. Then, the inward normal vector for each mesh node was calculated for the subsequent hemodynamics computation, which was based on the normal vectors of the adjacent triangular facets using the angle-weighted average method. The postprocessing flowchart is shown in *Figure 3*. The postprocess was similar to the method of MR fluid dynamics reported and validated in previous studies by Petersson *et al.* (25) and Isoda *et al.* (26).

The preprocessing steps of 4D flow MRI included eddy current correction and velocity mask application. After preprocessing and vessel wall surface smoothing, the WSS denoting the frictional force of blood shearing on the vessel wall was calculated with the following formula when considering blood as a Newtonian fluid:

$$WSS = \mu \left( \frac{\partial v}{\partial x} \right)_{x=0} \tag{1}$$

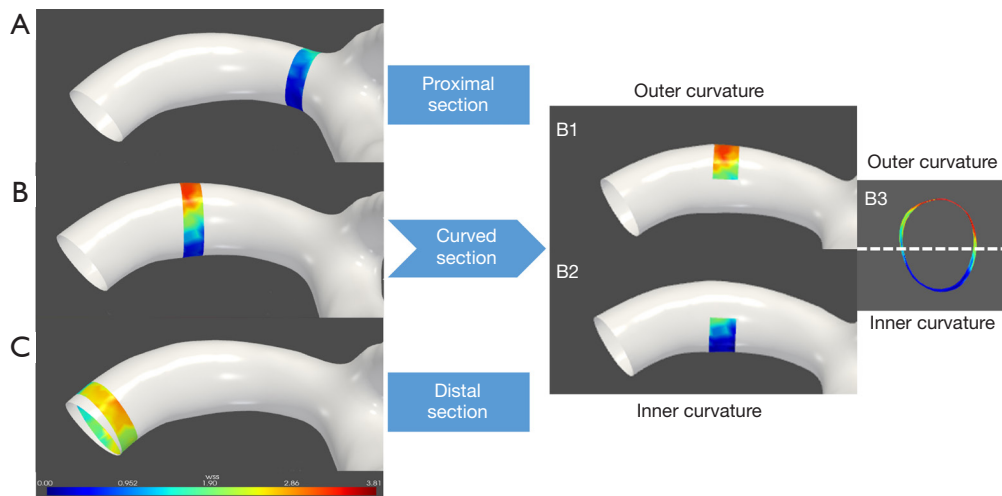
where  $\mu$  is the dynamic viscosity,  $v$  is the velocity parallel to the vessel wall, and  $x$  is the vertical distance from the vessel wall. Here, the velocity was estimated from a voxel (1 mm) at the wall and its adjacent voxel in the direction toward the center of the vessel, and the estimation of WSS was conducted based on a validated analysis method using parabolic fitting (25,26). Then, the time-averaged WSS (TAWSS) was calculated based on the obtained WSS within a cardiac cycle, as follows:

$$TAWSS = \frac{1}{T} \int_0^T |wss_i| dt \tag{2}$$

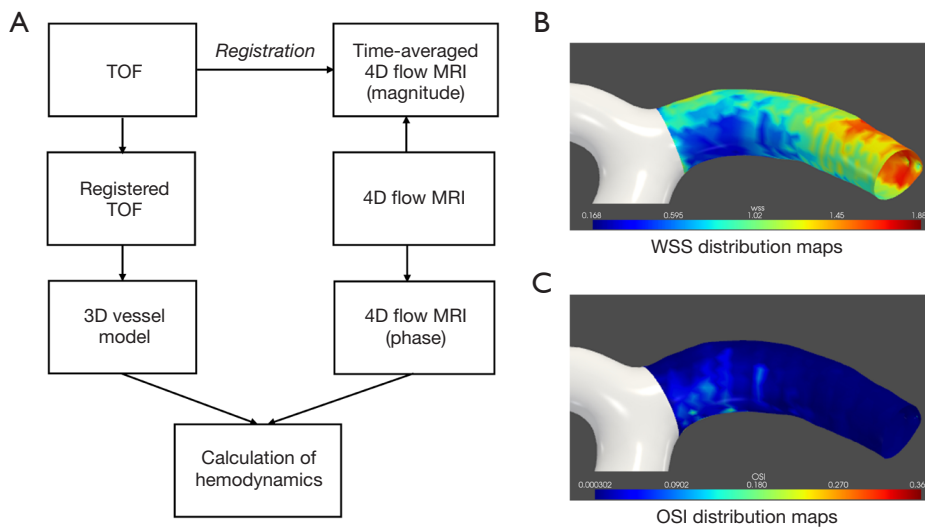
WSS oscillates during a cardiac cycle. Its degree of oscillation is described by the OSI, which can be calculated based on the WSS vector and its magnitude, as follows (25):

$$OSI = \frac{1}{2} \left( 1 - \frac{\left| \int_0^T wss_i dt \right|}{\int_0^T |wss_i| dt} \right) \tag{3}$$

where  $wss_i$  represents the instantaneous WSS vectors.



**Figure 2** Different sections along the long axis of the curved proximal (M1) segments. The M1 segment was divided into proximal (A), curved (B), and distal (C) sections, which were selected perpendicular to the long axis of the M1 segment for each section. For the curved M1 section, the circumferential wall was divided and described as the outer curvature (B1) and inner curvature (B2). At the cross-sectional plane of the curved M1 section (B3), the circumferential wall was divided into upper and lower halves by dashed lines, representing the outer curvature and inner curvature, respectively. The WSS distribution maps of the outer and inner curvature are also presented. WSS, wall shear stress.

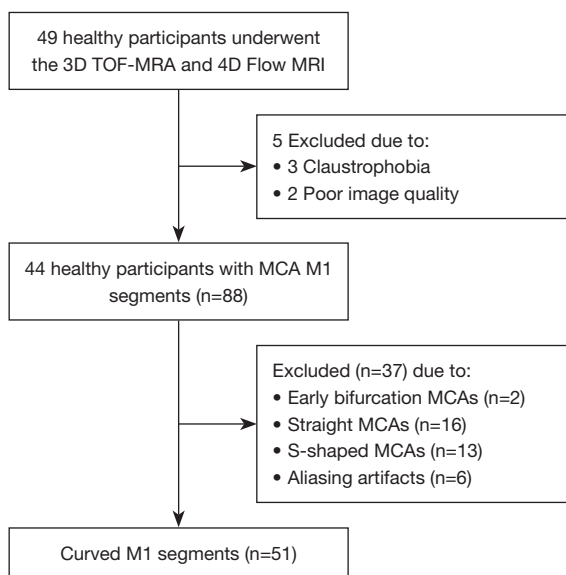


**Figure 3** Postprocessing and 3D visualization of 4D flow data. (A) The postprocessing flowchart is shown. After calculation, the visualized WSS (B) and OSI (C) distributions maps for the curved MCA are respectively presented. TOF, time-of-flight; MRI, magnetic resonance imaging; WSS, wall shear stress; OSI, oscillatory shear index; MCA, middle cerebral artery.

Here, the estimation of TAWSS and OSI using the abovementioned method was performed based on interpolated 4D flow MRI velocity data at a spatial resolution of 0.5 mm × 0.5 mm × 0.5 mm.

The hemodynamic parameters of the curved M1

segment of the MCA were analyzed. The WSS parameters, including mean TAWSS ( $TAWSS_{mean}$ , average value of all points on the targeted regional vessel), minimum TAWSS ( $TAWSS_{min}$ , minimum value of all points on the targeted regional vessel), maximum TAWSS ( $TAWSS_{max}$ , maximum



**Figure 4** The participants selection flowchart. 3D TOF MRA, three-dimensional time-of-flight magnetic resonance angiography; 4D flow MRI, four-dimensional flow magnetic resonance imaging; MCA, middle cerebral artery.

value of all points on the targeted regional vessel), and OSI parameters (maximum OSI ( $OSI_{max}$ ) were calculated for the circumferential wall of each location of each vessel. The coefficient of variation of TAWSS ( $TAWSS_{CV}$ ), which was used to quantify the non-uniformity of the spatial distribution of WSS on the targeted regional vessel, was calculated as follows, where  $TAWSS_{std}$  is the standard deviation of TAWSS on all spatial points and  $TAWSS_{mean}$  is the average value of those:

$$TAWSS_{CV} = \frac{TAWSS_{std}}{TAWSS_{mean}} \quad [4]$$

### Statistical analysis

The Shapiro-Wilk test was used to check normal distribution. Continuous variables were expressed as mean  $\pm$  standard deviation for normally distributed data and as median with range for the non-normally distributed data. Categorical variables were expressed as absolute or relative frequencies. Comparisons of the WSS and OSI parameters between the proximal and curved sections, proximal and distal sections, as well as the curved and distal sections of the curved M1 segments were performed by the Kruskal-Wallis H test due to the non-normally distributed data, and

all pairwise comparisons were performed using the Kruskal-Wallis one-way analysis of variance (ANOVA; k samples). Comparisons of the WSS and OSI parameters between the inner curvature and outer curvature of the curved M1 section were performed by the independent samples *t*-test for the normally distributed data and the Mann-Whitney U test for the non-normally distributed data. A P value <0.05 was considered statistically significant. All statistical analyses were performed using the SPSS 24.0 statistical software package (IBM Corp., Armonk, NY, USA).

### Results

The participant enrollment flow diagram is shown in Figure 4. Of the 49 healthy individuals enrolled in this study, 5 participants were excluded due to claustrophobia for MRI examination (n=3) and scans of poor image quality (n=2). Therefore, 44 healthy participants (18 males; mean age:  $27.16 \pm 5.69$  years; range, 20 to 51 years) with 88 M1 segments were included in this study. On the 3D TOF MRA, no abnormality was found in any participants. We excluded 37 M1 segments due to early bifurcation (defined as that occurring within 1 cm of the MCA origin) (n=2) (27), straight MCAs (n=16), S-shaped MCAs (n=13), and aliasing artifacts (n=6). Finally, 51 curved M1 segments were included in the analysis.

#### *Distribution variation of WSS and OSI at different sections of curved M1 segment*

The WSS and OSI parameters at different sections along the long axis of the curved M1 segment are listed in Table 2. A significant difference was found in the  $TAWSS_{min}$ ,  $TAWSS_{CV}$ , and  $OSI_{max}$  among the proximal, curved, and distal sections (all  $P < 0.01$ ). The curved M1 section had significantly lower  $TAWSS_{min}$  values than the proximal and distal sections ( $P = 0.031$  and  $P = 0.002$ , respectively) and the curved M1 section had significantly higher  $OSI_{max}$  values than the distal section ( $P = 0.001$ ). Furthermore, the  $TAWSS_{CV}$  values were found to be significantly different between the curved and proximal sections ( $P = 0.001$ ), as well as between the curved and distal sections ( $P < 0.001$ ) (Figure 5).

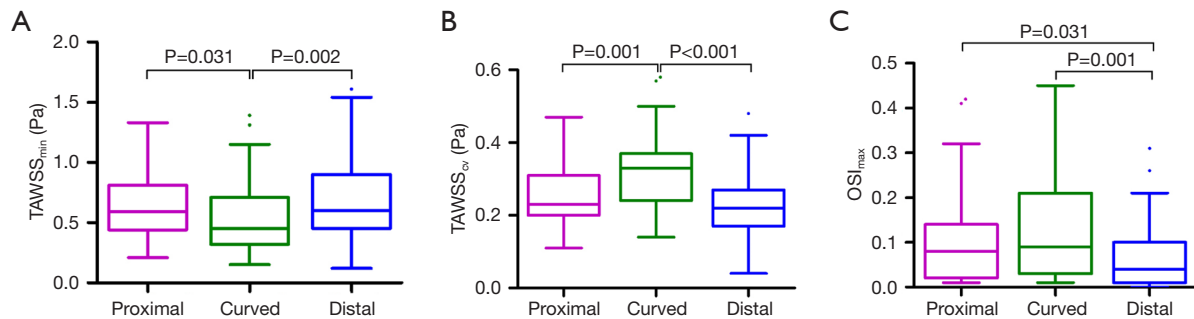
#### *Regional variation of WSS and OSI at inner and outer curvatures of curved M1 section*

The WSS and OSI parameters at the inner and outer

**Table 2** WSS and OSI parameters at different sections of the curved M1 segment

Parameters	Curved M1 segments (n=51)			P value
	Proximal	Curved	Distal	
WSS (Pa)				
TAWSS <sub>mean</sub>	1.39 (1.20–1.72)	1.33 (1.16–1.59)	1.36 (1.06–1.56)	0.708
TAWSS <sub>min</sub>	0.65 (0.46–0.85)	0.46 (0.34–0.74)	0.68 (0.48–0.93)	0.006**
TAWSS <sub>max</sub>	2.09 (1.90–2.35)	2.10 (1.91–2.64)	2.03 (1.65–2.29)	0.067
TAWSS <sub>CV</sub>	0.22 (0.19–0.30)	0.32 (0.24–0.36)	0.21 (0.16–0.27)	<0.001**
OSI				
OSI <sub>max</sub>	0.07 (0.02–0.11)	0.08 (0.03–0.21)	0.04 (0.01–0.10)	0.004**

Values are median (interquartile range). \*\*, indicates a statistical significance ( $P < 0.01$ ). WSS, wall shear stress; OSI, oscillatory shear index; TAWSS<sub>mean</sub>, mean values of time-averaged WSS; TAWSS<sub>min</sub>, minimum values of time-averaged WSS; TAWSS<sub>max</sub>, maximum values of time-averaged WSS; TAWSS<sub>CV</sub>, the coefficient of variation of time-averaged WSS; OSI<sub>max</sub>, maximum values of the oscillatory shear index; Pa, Pascal.



**Figure 5** Distribution variation of WSS and OSI parameters at different sections of the curved proximal (M1) segment. Comparisons of the TAWSS<sub>min</sub> (A), TAWSS<sub>CV</sub> (B), and OSI<sub>max</sub> (C) between the proximal and curved sections, the proximal and distal sections, as well as the curved and distal sections of the curved M1 segment in the box plots. A P value  $< 0.05$  was considered statistically significant. WSS, wall shear stress; OSI, oscillatory shear index; TAWSS<sub>min</sub>, minimum value of time-averaged WSS; TAWSS<sub>CV</sub>, the coefficient of variation of time-averaged WSS; OSI<sub>max</sub>, maximum value of oscillatory shear index.

curvatures of the curved M1 section are listed in *Table 3*. At the cross-sectional plane of the curved M1 section, it was found that the TAWSS<sub>mean</sub> ( $P = 0.002$ ), TAWSS<sub>min</sub> ( $P = 0.013$ ) and TAWSS<sub>max</sub> values ( $P = 0.015$ ) at the inner curvature were significantly lower than those at the outer curvature (*Figure 6*) and the OSI<sub>max</sub> values ( $P = 0.002$ ) at the inner curvature were significantly higher than those at the outer curvature.

## Discussion

In the current study, we reported the WSS and OSI parameters of curved M1 segments in healthy participants using 4D flow MRI. There were significant distribution and regional variation of the WSS and OSI parameters among

the different sections of the curved M1 segments, including the inner and outer curvatures of the curved M1 section.

Our results showed that the WSS and OSI values distributed along the long axis of the curved MCA were not uniform. In the curved M1 segment, the curved M1 section was found to have lower TAWSS<sub>min</sub> values than the proximal and distal sections and the curved M1 section was found to have higher OSI<sub>max</sub> values than the distal section. Since atherosclerotic plaque development is associated with regions exposed to low WSS and high OSI, our results might suggest that the curved M1 sections have hemodynamic features more conducive to atherosclerotic disease. The TAWSS<sub>CV</sub> is another interesting index used in our study to reflect the varying degree of TAWSS values

**Table 3** WSS and OSI parameters at outer and inner curvatures of the curved M1 section

Parameters	Curved M1 section		P value
	Outer curvature	Inner curvature	
WSS (Pa)			
TAWSS <sub>mean</sub>	1.49±0.37	1.26±0.51	0.002**
TAWSS <sub>min</sub>	0.75 (0.51–0.91)	0.51 (0.34–0.84)	0.013*
TAWSS <sub>max</sub>	2.13±0.44	1.91±0.57	0.015*
OSI			
OSI <sub>max</sub>	0.05 (0.02–0.07)	0.08 (0.04–0.17)	0.002**

Values were expressed as mean ± standard deviation or median (interquartile range). \*, indicates a statistical significance ( $P < 0.05$ ); \*\*, indicates a statistical significance ( $P < 0.01$ ). WSS, wall shear stress; OSI, oscillatory shear index; TAWSS<sub>mean</sub>, mean values of time-averaged WSS; TAWSS<sub>min</sub>, minimum values of time-averaged WSS; TAWSS<sub>max</sub>, maximum values of time-averaged WSS; OSI<sub>max</sub>, maximum values of the oscillatory shear index; Pa, Pascal.

among different locations along the circumferential wall. In our study, the curved M1 section demonstrated the highest TAWSS<sub>CV</sub>, significantly higher than both the proximal and distal sections. This morphological change may lead to a big difference in the WSS of the curvature region. The TAWSS<sub>CV</sub> was more sensitive in detecting unevenly distributed WSS values around the circumferential wall than other parameters.

In the current study, the inner curvature was found to have higher OSI and lower WSS parameters than the outer curvature of the curved M1 section. This certain shear force feature at the inner curvature of the curved vessel has also been demonstrated in many other vessels. Previous studies have reported that a vessel with geometric curvature demonstrates the obvious centrifugal flow pattern, with blood flow skewed to the outer curvature and reduced WSS at the inner curvature (28,29). The specific distribution feature of WSS and OSI at the curvature of vessels is probably related to the formation of vascular diseases. A flow-sensitive 4D MRI study on the aorta demonstrated that low WSS and a high OSI are distributed at the inner curvature and supra-aortic branch, which closely resembles the typical locations of atherosclerotic lesions (30). The predilection for plaque to be located at the inner curvature, both in U-shaped and inverted U-shaped MCAs (14) as well as the tortuous basilar artery, has also been defined by investigators (31). The results of the current study might

indicate possible underlying hemodynamic mechanisms for the formation and development of atherosclerotic cerebrovascular diseases.

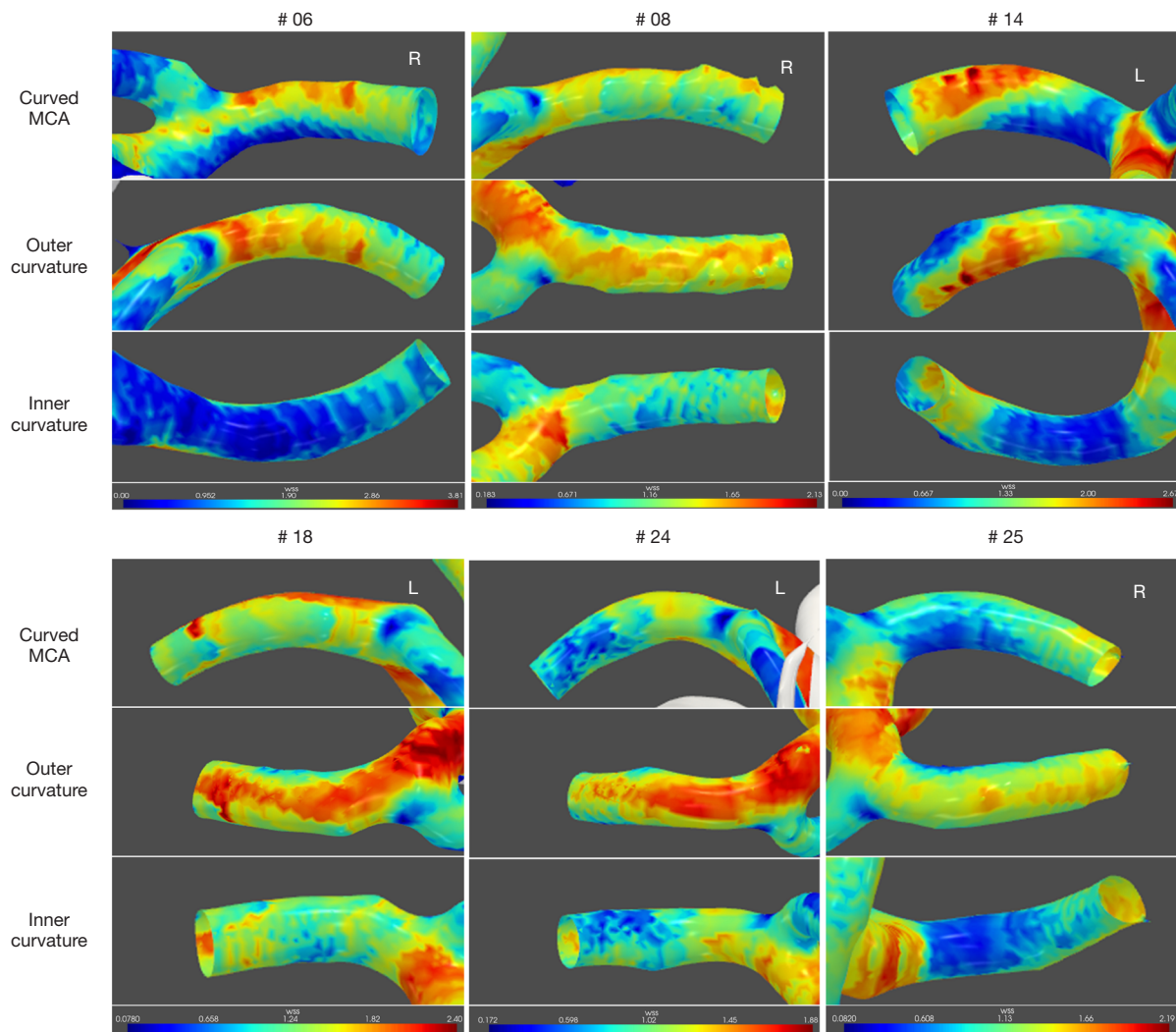
In this study, 4D flow MRI and TOF MRA images were integrated for the calculation and visualization of MCA hemodynamics. 4D flow imaging allows for direct *in vivo* measurement of 3D blood velocity, which can be utilized for the evaluation of hemodynamics, including WSS and the OSI (32,33). It could be considered as an *in vivo* individual assessment method for predicting the preferential locations of AS plaques or cerebral aneurysms. Furthermore, the TOF MRA images were used to segment and locate the boundary of a vessel as a supplement to the 4D flow MRI, due to the better signal contrast of blood flow in the TOF MRA images which improved the accuracy of vessel segmentation. The method used in the current study can also be applied in future studies to the hemodynamic assessment of intracranial arteries in other vascular diseases.

The 4D flow MRI has been gradually applied to the measurement of cerebrovascular hemodynamics, including intracranial atherosclerotic disease, intracranial aneurysms, and AVMs. Intracranial atherosclerotic plaques can alter local and global hemodynamics. Conversely, local hemodynamic status such as WSS may be related to AS plaque distribution and irregular plaque surface morphology (1,34). In a study of unruptured cerebral aneurysms, it was found that the average WSS and maximum blood flow correlated with the size of aneurysms (2). One hemodynamic study of AVMs showed that the WSS plays a vital role in vascular remodeling to monitor AVM response to treatment or understand other high-flow vascular pathologies (35). In recent years, the developments of highly accelerated 4D flow MRI (36) and multiple velocity encoding (multi-vec) (37) 4D flow MRI have resulted in increased flexibility of its application, which could be extended to the study of cerebrovascular diseases.

### Limitations

There were several limitations of the current study. First, the spatial resolution of the 4D flow sequence was set according to the recommendation (38). Approximately 3 voxels were acquired across the M1 segment using the spatial resolution of 1.0 mm × 1.0 mm × 1.0 mm. The number of voxels across the vessel of interest will increase with higher spatial resolution, which will help to improve the accuracy of the WSS calculation. Therefore, in this study, the interpolated 4D flow MRI data with a spatial





**Figure 6** The WSS distribution of the curved proximal (M1) segments in healthy participants. It showed that the minimum values of TAWSS were located at the inner curvature and the maximum values of TAWSS were located at the outer curvature of the curved M1 section. MCA, middle cerebral artery; WSS, wall shear stress; TAWSS, time-averaged WSS.

resolution of  $0.5 \text{ mm} \times 0.5 \text{ mm} \times 0.5 \text{ mm}$  were used to improve the hemodynamic evaluation. Also, as Ha *et al.* (39) have mentioned, accurate segmentation of the geometrical boundary of the vessel is essential for assessing the flow parameters on 4D flow MRI. In this study, the TOF MRA images were used for vessel segmentation. Although we think a higher contrast-to-noise ratio (CNR) might improve the accuracy of velocity calculations, the discrepancies between 4D flow MRI and TOF MRA-derived segmentation might be a very interesting topic for future study. Combining CFD models provides future direction for increasing the spatial resolution and further increasing

the WSS calculation accuracy based on the boundary condition of velocity measured by 4D flow MRI. Second, the sample size included in this study may not reflect the WSS distribution characteristics in a large population. The tortuosity of MCAs is more obvious in older patients (40). Given the relatively young age of our study participants, the results might have been affected by age bias. Furthermore, there may have been some potential operator bias in the measurements of quantitative metrics. In a future study, a quantitative method would be needed to verify the result in a group of participants of a larger sample size. Moreover, the WSS were presented as time-averaged values in this

study. Although the OSI was used to represent the temporal changes of WSS, the WSS distribution features at systolic, diastolic, or other phases of the cardiac cycle may provide more detailed information, which could help to better understand the hemodynamic mechanisms. Finally, only normal MCAs were studied. The investigation of the hemodynamics of stenosed MCAs would provide more information about AS-related hemodynamic features.

## Conclusions

According to our findings, there are distribution variation in the WSS and OSI parameters at the curved M1 section of curved MCAs, and the inner curvature of the curved M1 section has the lowest WSS and highest OSI distribution. The local hemodynamic features of the curved MCA may be related to the predilection for atherosclerotic plaque development.

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## Footnote

*Reporting Checklist:* The authors have completed the STROBE reporting checklist. Available at <https://qims.amegroups.com/article/view/10.21037/qims-22-67/rc>

*Conflicts of Interest:* All authors have completed the ICMJE uniform disclosure form (available at <https://qims.amegroups.com/article/view/10.21037/qims-22-67/coif>). The authors have no conflicts of interest to declare.

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