

3D printing technology applied to orthosis manufacturing: narrative review

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Abstract: Recently, three-dimensional (3D) printing technology has gradually been applied to the field of orthoses. This narrative review aimed to investigate the effect of 3D printed orthoses compared to conventional orthoses (non-3D printed orthoses). We searched MEDLINE for articles published up to July 27, 2020, and the main search phrases for identifying related articles were "3D printed orthosis", "3D printed orthoses", "3D printed braces", "3D printed splints", "3D printing orthosis", "3D printed orthoses", "3D printing braces" and "3D printing splints". We included articles that applied 3D printed orthoses to patients or healthy participants and excluded those not written in English, conference abstracts or presentations, and reviews. A total of 237 papers were identified, and qualifications were evaluated based on the title, abstract, and full text. A total of 22 articles were finally included in the analysis. The 3D printed orthoses showed similar or superior effects on biomechanical parameters and kinematic parameters such as wrist-hand function, wrist spasticity, arch height index, foot plantar pressure, and joint range of motion (ROM). In addition, 3D printed orthoses had high satisfaction and comfort compared to conventional orthoses. We believe that 3D printed orthoses can replace conventional ones, and they are expected to gain more popularity in the future.

Keywords: 3D printing technology; rehabilitation technology; orthosis; 3D printed orthosis

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Introduction

An orthosis is a device used to assist the functions of the human body. They usually have the following purposes: body protection, restricting motion, weight-bearing assistance, movement assistance, and deformity prevention or correction. Thus, orthoses are widely applied to patients with physical dysfunction and disability due to muscular dysfunctions, such as fractures, sprains, arthropathy and tendinopathy, and neurological disorders in the brain, spinal cord, and peripheral nerves (1,2). The conventional method for manufacturing orthoses is relatively time-consuming. Further, it is necessary to manually correct the shape and dimensions of the orthosis according to the patient's body. In addition, it is challenging to produce multiple customized orthoses with the same quality, and complex designs sometimes can be implemented. However, using recently developed three-dimensional (3D) printing technology, orthoses can be designed with exact dimensions through a computer graphic program, and the aforementioned disadvantages of the conventional method can be sufficiently addressed

Annals of Palliative Medicine, Vol 9, No 6 November 2020



Figure 1 Flow chart showing the search results for the study.

because 3D printers are highly accurate. Thus, using 3D printing technology, it is possible to design an orthosis with accurate numerical values of the dimensions through a design program and create structures that are difficult to implement manually (3-5). Additionally, while a manually produced orthosis requires approximately 1 week to produce, a 3D printer can perform this task in a day (6,7). Therefore, in the field of orthoses, significant attention is being paid to orthoses manufactured with 3D printing technologies.

In this study, we investigate the recent advancements in 3D printed orthoses by reviewing prior studies. We present this article in accordance with the narrative review reporting checklist (available at http://dx.doi.org/10.21037/ apm-20-1185).

Methods

We set "3D printed orthosis", "3D printed orthoses", "3D printed braces", "3D printed splints", "3D printing orthosis", "3D printed orthoses", "3D printing braces" and "3D printing splints" as keywords in PubMed, CINAHL Complete & MEDLINE Complete, Cochrane, Embase, and Scopus to search for articles published up to July 27, 2020. The criteria for article inclusion are as follows: (I) 3D printed orthosis applied to a patient or a healthy subject, (II) area of application should be an upper limb, lower limb, or spine, (III) prospective study, and (IV) the availability of a full-text. The criteria for article exclusion are as follows: (I) object of comparison is a surgical treatment, or a conservative treatment other than orthosis, (II) orthosis manufactured by adding electrical stimulation device or robotic device, (III) replacement product for human body structure made for surgery or implant, (IV) some parts produced by a 3D printer, and (V) case reports, conference abstracts or presentations, review articles, and non-English publications.

The level of evidence was defined using the Research Pyramid model. The evaluation criteria are as follows: (I) level 1: systematic reviews and meta-analysis of randomized controlled trials (RCTs), (II) level 2: one or more RCTs, (III) level 3: controlled trials without randomization (at least two groups), (IV) level 4: case-control or cohort study, (V) level 5: systematic review of descriptive and qualitative study, (VI) level 6: single descriptive or qualitative study, and (VII) level 7: expert opinion. The results of the level of evidence evaluation of the papers included in this review were level 2 in six papers (6-11), level 3 in six papers (4,5,12-15), and level 4 in ten papers (3,16-24).

Results

We identified 237 relevant articles. Among them, a total of 22 were selected (3-24), excluding articles that did not match the inclusion criteria (*Figure 1*). Of the 22

4264

studies, there were 8 studies related to the upper limbs (6,11,16-19,21,24), 13 related to the lower limbs (3-5,7-10,12,14,15,20,22,23), and 1 related to the spine (13). The characteristics of each study are summarized in *Table 1*. The following subsection explains how orthoses are made for each study.

Upper limb orthosis

Of the eight articles, two were randomized trials (6,11), and six were prospective observational studies (16-19,21,24).

In 2018, Kim et al. (6) manufactured a 3D printed orthosis in which the wrist joint was slightly dorsiflexed and free finger movements were possible, and the length was to the center of the forearm. The control group used ready-made cock-up splint. In 2020, Zheng et al. (11) manufactured the 3D printed orthosis in shape of a functional hand position (10°-15° extension of the wrist, 40°-45° flexion of the metacarpophalangeal (MP) and proximal interphalangeal, and thumb abduction). The control group used a low-temperature thermoplastic plate orthosis. In 2017, Chen et al. (16) 3D printed an orthosis designed to wrap around from the center of mid-forearm to the MP except for the thumb. In addition, the forearm part had several small holes for ventilation and wearerfriendliness, and the shells surrounding the upper and lower parts of the forearm-wrist-hand were sectioned and could be fixed using a Velcro strap. The 3D printed orthosis used by Portnova et al. (21) in 2018 was a wrist-driven orthosis, and each component of the orthosis was manufactured in various sizes to suit different users. The orthosis was designed with the feedback from three users and six orthotists. In 2018, Wang et al. (24) 3D printed the orthosis in the form of a fingerboard that straightens five fingers and maintains an abduction position. Small holes were drilled into the palmar side to make it breathable and comfortable for the user when wearing the orthosis. Only the base plate was produced using a 3D printer, and a Velcro strap was used for fixing it to the hand and finger. The 3D printed orthosis used by Guida et al. (18) had a design in which the wrists and hands were almost horizontally aligned, and the thumb was fixed at a slight abduction. The length of the body ranged from approximately proximal twothird of the forearm to a little above the MP. The shell was made in a double-shell design, and a hole was created on the entire shell for ventilation and lightness. In 2019, Lee et al. (19) 3D printed an orthosis designed to support from approximately the mid-forearm area to the MP and wrap only the MP area. The back of the hand and forearm were fixed with Velcro straps. As the patient wanted to perform daily life activities such as typing, eating, and writing. The hypothenar eminence area has a connector to fix a typing device or spoon, and a small ring was included between the thumb and index finger of the orthosis such that a pencil could be used. Furthermore, several small holes were made for breathability. In 2020, Chu et al. (17) measured the hands of 120 subjects and created a 3D parametric hand model. When manufacturing the orthosis, an offset of 1-2 mm was applied to the interphalangeal joint of the thumb and MP, and another offset of 2-3 mm was applied between the fifth metacarpal bone and the carpometacarpal joint. Thus, a suitable space was created on the inner surface between the thumb and the orthosis. This orthosis was designed to wrap under the MP, back of the hand, under the interphalangeal of thumb, and palm. There were no holes for ventilation, and because it consisted of one shell, a separate strap was not required.

Lower limb orthosis

Of the 13 related articles, there were four randomized trials (7-10) and 10 prospective observational studies (3-5,12,14,15,20,22,23).

In 2017, Telfer et al. (7) designed a 3D printed insole using foam-box foot impressions that were 3D scanned. The metatarsal area of the insole was layered, and the pressure was distributed when a vertical load was applied. The shape of the insole was similar to that of a ready-made insole. In 2019, Mo et al. (8) produced a 3D printed foot orthosis, with the subtalar joint positioned neutrally. A 3-mm PORON cover was added to the foot orthosis. Two studies were conducted in 2019 by Xu et al. (9,10). One of them was targeted at patients with plantar fasciitis (9). The pressure distribution was eased using lateral wedges in the heel of the insole and metatarsal pad. In a study involving patients with bilateral flat foot (10), a customized 3D printed insole was constructed that firmly supported the medial arch of the foot such that it did not collapse. In this 3D printed insole, the part surrounding the heel was deeper than in ready-made or normally customized insole, which increased the contact area where the foot touches the insole, thereby distributing the pressure. The 3D printed foot orthosis produced in two studies conducted by Telfer et al. in 2013 (22,23) were semi-rigid devices and threefourth of the total foot length. The 3D printed orthosis used by Dombroski et al. (4) was designed through a 3D

Annals of Palliative Medicine, Vol 9, No 6 November 2020

Table 1 Characteristics of included studies

4265

No.	Study	Study design	Participants	Applied body parts	Applied orthoses	Digital fabrication pathway	Type of 3D printer	Material of 3DP	Result
1	Kim <i>et al.</i> (6)	Randomized trial	N=22 (E: 11, C: 11), overuse syndrome in the upper wrist area	Upper limbs (wrist-hand)	3D printed wrist orthosis (3DP), cock-up splint (CO)	3D scanner	Fused filament fabrication [FINEBOT Z420 3D printer (TPC Mechatronics Inc., Incheon, Korea)]	Thermoplastic polyurethane	Pain and function: (I) patient-rated wrist (ii) CO: baseline: 28.8±4.8, after 1 wk: 23 (ii) CO after 1 wk: 1.0±6.8. Satisfaction: statistically significant difference in the 3
2	Zheng <i>et al.</i> (11)	Randomized trial	N=60 (E: 30, C: 30), Colles' fractures	Upper limbs (wrist-hand)	3D printed wrist-hand orthosis (3DP), manually produced small splint (low-temperature thermoplastic plate orthosis, CO)	CAD	Nonexistent information	Light-activated resin	Spasticity/stability, mobility, hand function assessment score/visual analog scale/s mean 1.6/5.2/2.5/1.0; (II) CO: baseline: n
3	Chen <i>et al.</i> (16)	Prospective observational study	N=10, distal radius fracture	Upper limbs (wrist-hand)	3D printed cast	Magnetic resonance imaging and computerised tomography	Selective laser sintering (EOS P395, Germany)/stereolithography printer (RS4500, UnionTech, China)	Polypropylene and polyamide	Clinical efficacy (stability, blood circulati 15 points
4	Portnova <i>et</i> <i>al.</i> (21)	Prospective observational study	N=3, spinal cord injury	Upper limbs (wrist-hand)	3D printed wrist-driven orthosis	CAD	Fused filament fabrication (FlashForge Creator Pro, FlashForge, Rowland Heights, CA, USA)	Polylactic acid plastic	Average score of function/aesthetics/co 1: improvement in cards, small objects, writing, eating, checkers, empty cans, a objects, and checkers sections
5	Wang <i>et al.</i> (24)	Prospective observational study	N=18, stroke	Upper limbs (hand)	3D printing fingerboard	3D scanner	Fused deposition modeling	Polylactic acid	Pain: visual analog scale: before: 2.0±1. strength: hand grip dynamometer: befor ROM of hand joints: (I) wrist flexion (activ (II) wrist extension (active): before: 1.0±2 of the hand: modified Ashworth scale: b Hand movement function: Brunnstrom a 3.23±0.83
6	Guida <i>et al.</i> (18)	Prospective observational study	N=18, nondisplaced metaphyseal distal fractures of the radius	Upper limbs (wrist-hand)	3D printed cast	3D scanner	Fused deposition modeling	Thermoplastic modified acrylonitrile butadiene styrene	Pain: (I) visual analog scale: before/after (pain section): before/after treatment: 24 (functionality section): before/after treatment
7	Lee <i>et al.</i> (19)	Prospective observational study	N=1, stroke	Upper limbs (wrist-hand)	3D printed wrist-hand orthosis (3DP), ready-made assistive device (CO)	3D scanner	Fused filament fabrication [FB9600 printer (TPC Mechatronics Inc., Incheon, Korea)]	Thermoplastic polyurethane (3DP), polylactic acid (connector)	Jebsen hand function test (writing/feedi user assessment (writing/feeding/typing
8	Chu <i>et al.</i> (17)	Prospective observational study	N=1, healthy	Upper limbs (hand)	3D hand orthosis	3D scanner	Fused deposition modeling (Grandore Fika 2: Stratasys, Eden Prairie, MN, USA)	Thermoplastic elastomer	Usability test: possible to unscrew a bol a smartphone. Quebec user evaluation of
9	Telfer <i>et al.</i> (7)	Randomized trial	N=20 (E:20, C:20), diabetes	Lower limbs (foot)	3D printed insole, standard insole	3D scanner	Fused deposition modeling [Airwolf HD2x printer (Airwolf 3D, Costa Mesa, CA, USA)]	Polyethylene acetate	Peak pressure result (kPa): (I) 3D printed approximately 245
10	Mo <i>et al.</i> (8)	Randomized trial	N=13 (E: 13, C: 13), asymptomatic runners with excessive foot pronation	Lower limbs (foot)	3D printed foot orthosis (3DP), traditional plaster molded (TPM)	3D scanner	Nonexistent information	Nylon (Polymarker PolyMide [™])	* mean values of 3DP/TPM. Rearfoot ev angle (°): 7.0/6.5. Rearfoot eversion velo eversion velocity (degrees/s): 163.2/149 instantaneous loading rate (BW/s): 73.0, Perceived comfort score on heel cushio
11	Xu <i>et al.</i> (9)	Randomized trial	N=60 (E: 30, C: 30), plantar fasciitis	Lower limbs (foot)	3D printed insole (3DP), prefabricated insole	CAD	Fused deposition modelling (Bodyarch X1 printer®)	Polyethylene acetate	Pain: visual analog scale: (I) 3DP: baseli baseline: 8.72±3.93, after 8 wk: 5.25±1.
12	Xu <i>et al.</i> (10)	Randomized trial	N=80 (E: 40, C: 40), bilateral flatfoot	Lower limbs (foot)	3D printed insole (3DP), prefabricated insole	CAD	Fused deposition modelling (Bodyarch X1 printer®)	Polyethylene acetate	Pain: visual analog scale: (I) 3DP: baseli baseline: 8.12±1.21, after 8 wk: 5.92±1.

Table 1 (continued)

t evaluation: (i) 3DP: baseline: 29.3±8.6, after 1 wk: 19.2±6.2; 23.4±6.9; (II) Jebsen hand function test: (i) 3DP: after 1 wk: 4.3±6.9; c orthotics and prosthetics user survey: high satisfaction score with 3DP group (P=0.036)

ion/pain/swelling: modified Ashworth scale (wrist flexor)/Fugl-Meyer swelling score: (I) 3DP: baseline: mean 2.2/3.9/3.0/3.0, after 6 wk: mean 2.2/3.9/3.0/2.5, after 6 wk: mean 2.0/4.1/3.0/2.0

ion, pain, pressure): 9.8 out of 12 points. Satisfaction: 11.5 out of

omfort from user: 6.8/7.7/7.7. Jebsen hand function test: (I) patient , checkers, and empty cans sections; (II) patient 2: improvement in and full cans sections; (III) patient 3: improvement in writing, small

.58, after 3 wk: 1.85±1.34, after 3 mo: 1.69±1.03. Hand grip ore: 0.018±0.041, after 3 wk: 0.025±0.054, after 3 mo: 0.032±0.067. ive): before: 2.62±8.27, after 3 wk: 5.08±11.6, after 3 mo: 5.83±13.8; 2.77, after 3 wk: 3.62±9.83, after 3 mo: 3.85±11.2. Muscle tension before: 2.38±0.65, after 3 wk: 2.31±0.48, after 3 mo: 1.73±0.70. approach: before: 2.77±0.83, after 3 wk: 3.00±0.82, after 3 mo:

r treatment: $5.70\pm3.20/0.22\pm0.65$; (II) patient-rated wrist evaluation $4.00\pm16.00/4.30\pm5.60$; (III) patient-rated wrist evaluation ment: $22.00\pm03.00/4.3\pm4.00$

ling/typing) (s): 3DP: 43.2/12.3/22.3; CO: 42.6/25.1/24.2. Quebec g) (s): 3DP: 31/35/38; CO: 30/28/30

ottle cap, handwrite, play computer game with a mouse, and text on of satisfaction with assistive technology: mean satisfaction level: 4.9

d insole: approximately 285; (II) standard shaped insole:

version angle at initial contact (°): 3.3/3.1. Peak rearfoot eversion ocity at initial contact (degrees/s): 118.0/105.6. Peak rearfoot 9.0. Vertical average loading rate (BW/s): 54.5/54.8. Vertical 0/70.2. Perceived comfort score on medial-lateral control: 6.2/6.5. oning: 6.1/6.9

line: 7.34 \pm 3.43, after 8 wk: 3.12 \pm 0.51; (II) prefabricated insole: .22

ine: 7.91±3.11, after 8 wk: 2.42±0.13; (II) prefabricated insole: .19

Table 1 (continued)

No.	Study	Study design	Participants	Applied body parts	Applied orthoses	Digital fabrication pathway	Type of 3D printer	Material of 3DP	Result
13	Telfer <i>et al.</i> (22)	Prospective observational study	N=24 (E: 12, C: 12), pronated foot	Lower limbs (foot)	3D printed foot orthosis	3D scanner	Fused deposition modeling [3D printing system (RapMan; Bits from Bytes, Clevedon, UK)]	Polyactide	Significant linear effect in plantar pres peak/mean lateral forefoot: P<0.001
14	Telfer <i>et al.</i> (23)	Prospective observational study	N=24 (E: 12, C: 12), pronated foot	Lower limbs (foot)	3D printed foot orthosis	3D scanner	Fused deposition modeling [3D printing system (RapMan; Bits from Bytes, Clevedon, UK)]	Polyactide	Significant linear effect in kinematic a mean internal tibial rotation: P=0.003; adduction moment: P<0.001; mean ki
15	Dombroski <i>et al.</i> (4)	Prospective observational study	N=1, healthy (without lower extremity injuries)	Lower limbs (foot)	3D printed foot orthosis (3DP), plaster casted orthosis, shod condition	3D scanner	Fused deposition modeling [desktop 3D printer (Makerbot [®] , Makerbot Industries, Brooklyn, NY, USA)]	Acrylonitrile butadiene styrene filament	Arch height index (mm): 3DP: 21.5±0.
16	Allan e <i>t al.</i> (12)	Prospective observational study	N=20 (E: 10, C: 10), symptomatic medial knee osteoarthritis	Lower limbs (foot)	Eight types of 3D printed insole with lateral wedging—types: 3/4 length or full length with 0° (A), 5° rearfoot (B), 10° rearfoot and 5° forefoot (C), and 10° rearfoot (D), respectively	3D scanner	Fused deposition modelling [desktop 3D printing system (3D Touch; Bits from Bytes, Clevedon, UK)]	Soft polylactide thermoplastic	Percentage changes in biomechanica effects in length and wedging condition moment: significant main effects in len (III) knee adduction moment impulse: and P<0.0001
17	Cha e <i>t al.</i> (3)	Prospective observational study	N=1, foot drop	Lower limbs (ankle-foot)	3D printed ankle-foot orthosis (3DP), conventional Ankle-foot orthosis	3D scanner	Fused filament fabrication (FB9600 [®] , TPC Mechatronics Corp., Incheon, Korea)	Thermoplastic polyurethane	Gait speed (cm/s): 3DP/conventional A AFO/no AFO: 70.9/70.9/63.2. Step wi stance ratio between the right/left side evaluation of satisfaction with assistiv
18	Jin <i>et al.</i> (5)	Prospective observational study	N=30, healthy	Lower limbs (foot)	3D printed insole with arch lift (A), 3D printed insole (B), standardized pre-made insole (C)	3D scanner	Fused deposition modelling (Bodyarch X1 printer®)	Polyethylene acetate	Peak pressure in rearfoot (kPa): A/B/C A/B/C: approximately 22/25/35. Rang (A/B/C): approximately 2.8/4/4; foot fl lateral center of pressure (cm/s): foref
19	Liu <i>et al.</i> (20)	Prospective observational study	N=12, stroke	Lower limbs (ankle-foot)	3D printed ankle-foot orthosis (3DP)	3D scanner	Multi Jet Fusion (Jet Fusion 3D 4200, HP, USA)	3D high reusability polyamide 12	Temporal-spatial parameters (before/a (times/min): 47.0±14.4/53.8±15.5; stri double limb support phase (%): 36.3±
20	Mannisi <i>et al.</i> (14)	Prospective observational study	N=7, knee osteoarthritis	Lower limbs (foot)	Three types of 3D printed insole with 0°, 5°, and 10° of lateral wedge	3D scanner	Fused deposition modelling (desktop 3D printing system (Airwolf 3D HDx, Airwolf 3D printers, California, U.S.A.))	Soft thermoplastic polyactic acid	Medial to lateral ratio for the impulse (2.68/2.93/2.80/2.75. Walking speed (r
21	Tarrade <i>et al.</i> (15)	Prospective observational study	N=34, standing workers with foot pain	Lower limbs (foot)	3D printed custom-made foot orthosis	3D scanner	Laser sintering	Polyamide 12	Numerical rating scale (pain/comfort/l 2.0 \pm 2.0/1.4 \pm 2.1/2.1 \pm 2.4. Foot health before 3DP: 59.5 \pm 28.5/69.9 \pm 24.6/37.1 6/59.0 \pm 25.0. Center of pressure parar 1,370.6 \pm 380.6/1,682.9 \pm 937.6; amplitu amplitude of medial-lateral displacem (mm/s): 17.7 \pm 5.7/19.8 \pm 15.3; mean me COP position) (mm ²): 397.5 \pm 755.2/46
22	Kuo <i>et al.</i> (13)	Prospective observational study	N=41, healthy	Spine (cervical)	3D printed customized collar (3DP), Aspen Vista collar, Sport-aid cervical collar	3D scanner	Fused deposition modelling	Biodegradable polylactide	Head/neck/trunk angle [mean value (° without back support: 24.36/18.74/14 support: 13.81/6.85/1.07, sitting witho (III) sport-aid: sitting with back suppor standing: 21.41/3.84/10.88

E: number of patients in experimental group; C: number of patients in control group. 3DP, 3D printed orthosis; CO, conventional orthosis; MP, metacarpophalangeal; PIP, proximal interphalangeal; ROM, range of motion; TPM, traditional plaster-molded foot orthosis; AFO, anklefoot orthosis; COP, center of pressure; TMO, traditional mold-based orthosis.

4266

ssure: mean lateral rearfoot: P=0.001; peak/mean midfoot: P<0.001;

nd kinetic variables: peak/mean rearfoot eversion: P<0.001; ; peak/mean ankle eversion moment: P<0.001; second peak knee anee adduction moment: P<0.001

.96; plaster casted orthosis: 22.0±0.84; shod condition: 21.2±0.83

al variables: (I) first peak knee adduction moment: significant main on except A: P=0.038 and P<0.0001; (II) second peak knee adduction ength and wedging condition: P=0.018 and P<0.0001; significant main effects in length and wedging condition: P=0.022

AFO/no AFO: 56.5/56.5/42.2. Stride length (cm): 3DP/conventional idth (cm): 3DP/conventional AFO/no AFO: 15.9/17.1/17.9. Single les (%): 3DP/conventional AFO/no AFO: 80.4/79.7/69.7. Quebec user ve technology 3DP/conventional AFO: 4.5/4.1

C: approximately 170/200/260. Force-time integral in forefoot (%): ge of medial-lateral center of pressure (mm): forefoot contact phase lange phase (A/B/C): approximately 3.1/5/5.1. Velocity of medialfoot contact phase (A/B/C): approximately 15/16/19

after using 3DP): velocity (m/s): $0.17\pm0.06/0.20\pm0.07$; cadence ide length (m): $0.43\pm0.11/0.48\pm0.11$; gait cycle (s): $2.8\pm1.1/2.5\pm1.0$; $\pm5.6/33.6\pm5.2$; step length difference (m): $0.16\pm0.12/0.10\pm0.09$

of the compressive force: shoe only: $0^{\circ}/5^{\circ}/10^{\circ}$; mean: m/s): shoe only: $0^{\circ}/5^{\circ}/10^{\circ}$; mean: 1.15/1.15/1.18/1.17

/heavy legs): before 3DP: $5.3\pm2.4/5.9\pm2.8/5.3\pm3.1$, after 3DP: status questionnaire (pain/function/footwear/general foot health): $.0\pm24.5/38.5\pm27.6$, after 3DP: $85.1\pm18.7/92.8\pm15.2/47.3\pm27$. imeters (with/without 3DP): total displacement of sway (mm): tude of anteroposterior displacement (mm): $30.8\pm17/40.4\pm26.5$; nent (mm): $20.1\pm9.7/30.4\pm15.9$; mean anteroposterior velocity redial-lateral velocity (mm/s): $16.7\pm4.5/21.9\pm11.2$; sway area (95% of 52.9 ± 659.8

^o)]: (I) 3DP collar: sitting with back support: 12.25/5.31/0.03, sitting 4.49, standing: 13.9/3.26/11.73; (II) Aspen Vista: sitting with back out back support: 29.57/22.74/15.87, standing: 15.24/3.51/11.25; rt: 20.49/7.29/0.2, sitting without back support: 32.94/21.53/14.52,

scan. Although the shape was not specifically mentioned, it had a feature that resulted in a higher arch height index than the control group. Allan et al. (12) evaluated the effect using eight types of 3D printed insole, including three-fourth of the length or full length with (I) 0° rearfoot, (II) 5° rearfoot, (III) 10° rearfoot and 5° forefoot, and (IV) 10° rearfoot. All individuals' foot were scanned, and the insoles were made according to the shape of each foot. The orthosis used by Cha et al. (3) was an open type of heel and malleolus. Similar to the conventional orthosis, the front side was open with a shape that wrapped more to the front of the lower limb. The calf shell and plantar foot-plate length were approximately half of the conventional orthosis. In 2019, Jin et al. (5) produced the basic 3D printed insole in the form of a raised heel structure and an arched arch lift. The experimental group was divided into two groups; Group A had modified insoles such that the lateral-longitudinal portion was completely in contact with the bottom. The insoles of Group B were not applied with an arch lift. Liu et al. (20) produced 3D printed ankle-foot orthosis similar to posterior leaf spring orthosis. The ankle trim line passed behind the malleolus, and the foot plate fitted the entire length of the plantar of the foot. The sole and calf shells had several holes for comfort, ease of ventilation, weight reduction, and material cost savings. The 3D printed insole used by Mannisi et al. (14) was produced by adding lateral wedges of 0°, 5°, and 10° to the insoles manufactured by 3D scanning the knees and ankles at a 90°-bend with no load applied. Tarrade et al. (15) scanned each patient's foot through a 3D footprint scanner and made customized orthoses. Subsequently, neutral insole was attached to the foot orthosis and applied to the subjects. Foot orthoses had an arch shape to support the arch.

Spinal orthosis

One prospective observational study was conducted to evaluate the effectiveness of 3D printed spinal orthosis (13).

The 3D printed orthosis used by Kuo *et al.* (13) was applied to the cervical vertebrae. Typical cervical orthosis wraps around the entire neck, whereas the 3D printed orthosis used in that study had support only in the front side. There were mandibular and lateral supports that descended to the clavicle at both ends of the mandibular support. In addition, the 3D printed orthosis had venting holes and strap holes on the mandibular support. The user could be fixed using the strap to prevent the orthosis from falling off the body.

Discussion

In the current review, we found that 3D printed orthoses can effectively improve biomechanical and kinematic parameters, and their effectiveness is similar to that of conventional orthoses. Additionally, study participants felt comfortable wearing 3D printed orthoses. Furthermore, in some studies, the effectiveness of 3D printed orthoses and the comfort when wearing them were better than those of conventional orthoses. Of the 22 studies included in our review, 10 of them (3-5,7-11,13,19) compared the effectiveness of 3D printed orthoses with that of conventionally produced orthoses. In all those studies, 3D printed orthoses showed superior or similar results in the evaluation parameters (satisfaction, wrist spasticity, wristhand function, gait parameter, arch height index, and plantar foot pressure and joint range of motion (ROM) compared to conventional orthoses, and patient satisfaction with 3D printed orthoses was also comparable with that of conventional orthoses. The reasons why 3D printed orthoses were more satisfactory and some explanations are as follows:

(I) The surface of the body in contact with the orthosis is optimized in 3D-printed orthoses.

Most conventional orthoses are made manually. Even if the orthosis is produced based on the patient's body casting, human error should not be overlooked. In particular, a slight difference in force can affect the metal orthoses when bending the stirrup or upright. In plastic orthosis, while making the negative plaster model, the plaster cloth wraps around the patient's body, which may create parts where the flesh is pressed and uneven. In addition, the conventional orthoses are worn by the patient after manufacture, and the operations of finely adjusting the angle, alignment, or circumference can be performed again. In contrast, the 3D printed orthoses are designed using computer programming and produced through a 3D printer. If the producer has accurate body dimensional information, there is a high probability that the output will be highly accurate.

 (II) More solid support of patients' bodies than conventional orthoses, because the materials (polyurethane, light-activated resin, etc.) used in 3D printed orthoses have higher strength, which leads to better effects on controlling the ROM of joints. Strength refers to the resistance until the material breaks down. The strength decreases as the number of repeated and continuous loads to the orthosis increases. Therefore, it is important to consider the strength of the material when manufacturing an orthosis. However, strength is not the only factor to consider. In the case of an ankle-foot orthosis, if users wear an orthosis during gait, the impact on the orthosis every time they walk can be a problem. Therefore, toughness and brittleness, which are the characteristics of impact resistance, should be considered. In addition, as the plastic orthosis for the purpose of correction is applied with a continuous load, the orthosis may deform over time. In this case, creep and relaxation, which are the characteristics related to strain over time, should be considered.

(III) Increased comfort owing to the good distribution of pressure.

The distribution of pressure is influenced by a number of variables, including the shape of the body, size of the orthosis, structure of the orthosis, and motion of the affected area. The bone protrusion part or affected area needs space to avoid contact with the orthosis. If the orthosis is small and an excessive pressure is applied, adjustment is required. In the case of a flat foot, the load to the arch can be distributed by applying an arch support to the insole. The medial/lateral wedge or pad has the same function. The pressure is directly related to the user's comfort; therefore, it is important to consider it when designing an orthosis.

(IV) Lighter weight than conventional orthoses.

The weight of the orthosis is not limited to the selection of main material. By using 3D printing technology, the weight can be reduced with great precision by making small holes on the narrow surface. Making holes in the orthosis reduces weight and provides ventilation. In addition, designing to omit bolts, nuts, metal rings, etc., or outputting parts to a 3D printer can help reduce the weight of the orthosis.

The effects and satisfaction of 3D printed orthosis were also evaluated in studies not mentioned previously (6,12,14-18,20-24). The results of stability, pain, pressure, function of the affected area, and satisfaction were generally excellent (*Table 1*). In aggregate, the pain was reduced, joint ROM was improved, and satisfaction was high because it was light and comfortable to wear. Given the advantages of 3D printed orthoses, this technology is expected to be used more widely in clinical practice in the near future. However, 3D printed orthosis is not excellent in all aspects. When performing a 3D scan, difficulty may arise owing to the patient being in an incorrect posture or continuously moving. In this case, a posture correction device should be used or an expert should set the optimal posture. There are limitations of the 3D printer as well. It is difficult to manufacture an orthosis with an exceptionally large circumference or height. In addition, although the price range varies, a printer with excellent quality and high production speed is expensive; therefore, it may be difficult to obtain a machine without basic funds. The use of unwarranted, low-cost printer and materials requires caution as it can cause secondary damage to users. In addition, for 3D printing technology to be actively used in the manufacturing of orthoses, we expect that practitioners in related fields, such as clinicians, prosthetists, orthotists, and occupational therapists, will have to acquire CAD utilization skills and increase their understanding of 3D printing technology.

Among the 22 studies included in our review, in 15 of them (3-8,12-15,18-20,22,23), the subjects' bodies were scanned using a 3D scanner and later a CAD program was used to handle the data and design the orthosis. In five studies (9-11,17,21), a CAD program was directly used to design the orthosis, which was then self-produced. CAD files obtained through a 3D scanner can be modified using a CAD program, which is a design program that is used to create and edit drawings. Because CAD files can be stored for a long time, it is easy to manufacture an orthosis of the same design using a saved file when the orthosis is damaged or lost (3,11). It is also easy to modify it according to the patient's desired shape (9,19). Open-source design is a free design source. It is free to use and accessible by anyone, and a wider variety of designs can be created in a short period of time based on open-source data (21).

The materials usually used for 3D printed orthoses include PLA, ABS, and TPU. PLA is an environmentally friendly material that has no environmental hormones or heavy metals. Additionally, PLA is a material with excellent renewability and biocompatibility (25). ABS is a type of styrene resin composed of three components (acrylonitrile, butadiene, and styrene). ABS has high impact resistance and ease of processability (26). TPU has mechanical properties, such as the highest tensile strength, tearing strength, and abrasion resistance among thermoplastic elastomers (26).

Annals of Palliative Medicine, Vol 9, No 6 November 2020

Therefore, these materials are being widely used when manufacturing objects with high durability.

In this review, we investigated the effects of 3D printed orthoses. In all reviewed studies, 3D printed orthoses were durable and showed similar or superior results in biomechanical parameters, kinematic parameters, and comfort evaluation compared to conventional orthoses. Based on these results, 3D printed orthoses appear to be of sufficient value to replace conventional orthoses in clinical practice. However, previous studies had a small percentage of randomized trials and fewer results comparing conventional and 3D printed orthoses. In particular, for a spinal orthosis, there is only one prospective observational study. In addition, some studies only confirmed satisfaction, which is an individual's subjective indicator. Therefore, for 3D printed orthoses to be more actively utilized in clinical practice, more randomized trials should be conducted to minimize the risk of bias and ensure the validity of the study. Moreover, it is necessary to compare the effects of conventional orthosis and 3D printed orthosis and evaluate objective indicators such as joint ROM, pressure distribution, and kinematic data.

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Footnote

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